TRANSMISSION LINE THEORY

(TEM Line)

A uniform transmission line is defined as the one whose dimensions and electrical properties are identical at all planes transverse to the direction of propagation.

Circuit Representation of TL's

A uniform TL may be modeled by the following circuit representation:



R: Series resistance per unit length of line (for both conductors (ohm/m)).

L: Series inductance per unit length of line (Henry/m).

G: Shunt conductance per unit length of line (mho/m).

C: Shunt capacitance per unit length of line (Farad/m).

The line is pictured as a cascade of identical sections, each of Δz long.

Since $\Delta z \text{ can always be chosen small compared to the operating wavelength, an individual section of line may be analyzed using ordinary ac circuit theory. In the following analysis, we let <math>\Delta z \rightarrow 0$, so the results are valid at all frequencies (hence for any physical time variation).

Applying the Kirchhoff's voltage law to the line section gives:

$$v(z,t) = (R\Delta z)i(z,t) + (L\Delta z)\frac{\partial i(z,t)}{\partial t} + v(z+\Delta z,t)$$

Rearranging yields:

$$\frac{v(z + \Delta z, t) - v(z, t)}{\Delta z} = -R \ i(z, t) - L \frac{\partial i(z, t)}{\partial t}$$

Letting $\Delta z \rightarrow 0$, we get,

$$\frac{\partial v(z,t)}{\partial z} = -R \ i(z,t) - L \frac{\partial i(z,t)}{\partial t}$$

Now applying Kirchhoff's current law to the line section gives:

$$i(z,t) = (G\Delta z)v(z + \Delta z, t) + (C\Delta z)\frac{\partial v(z + \Delta z, t)}{\partial t} + i(z + \Delta z, t)$$

Rearranging yields:

$$\frac{i(z+\Delta z,t)-i(z,t)}{\Delta z} = -G \ v(z+\Delta z,t) - C \frac{\partial v(z+\Delta z,t)}{\partial t}$$

Letting $\Delta z \rightarrow 0$

$$\frac{\partial i(z,t)}{\partial z} = -G v(z,t) - C \frac{\partial v(z,t)}{\partial t}$$

Then the time domain TL or telegrapher equations are:

$$\frac{\partial v(z,t)}{\partial z} = -R \ i(z,t) - L \frac{\partial i(z,t)}{\partial t}$$
$$\frac{\partial i(z,t)}{\partial z} = -G \ v(z,t) - C \frac{\partial v(z,t)}{\partial t}$$

The solution of these equations, together with the electrical properties of the generator and load, allow us to determine the instantaneous voltage and current at any time t and any place z along the uniform TL.

Lossless Line: For the case of perfect conductors (R=0) and insulators (G=0), the telegrapher equations reduce to the following form:



$$-L\frac{\partial}{\partial t}\left(\frac{\partial i(z,t)}{\partial z}\right) = -L\frac{\partial}{\partial t}\left(-C\frac{\partial v}{\partial t}\right)$$

Or,



Wave equation's for voltage and current on a lossless TL.

Although real lines are never lossless, lolessness approximation for practical TL's is very usefull.

TRANSMISSION LINES WITH SINUSOIDAL EXCITATION

We will only consider the sinusoidal steady-state solutions.

Transmission-Line Equations:

Under sinusoidal steady state conditions, the TL equations take the form:

$$\frac{dV(z)}{dz} = -(R + j\omega L)I(z)$$
$$\frac{dI(z)}{dz} = -(G + j\omega C)V(z)$$

Where V(z) and I(z) are voltage and current phasors.

The real sinusoidal voltage and current waveforms are obtained from:

$$v(z,t) = \operatorname{Re}\left[V(z)e^{j\omega t}\right]$$
$$i(z,t) = \operatorname{Re}\left[I(z)e^{j\omega t}\right]$$

Wave Propagation on a TL

The second order differential equations for V(z) and I(z) are:

$$\frac{d^2 V(z)}{dz^2} - \gamma^2 V(z) = 0$$
$$\frac{d^2 I(z)}{dz^2} - \gamma^2 I(z) = 0$$

where $\gamma = \alpha + j\beta = [(R + j\omega L)(G + j\omega C)]^{1/2}$

 $\gamma =$ complex propagation constant.

 α = attenuation constant (Np/m).

 β = phase constant (rad/m).